



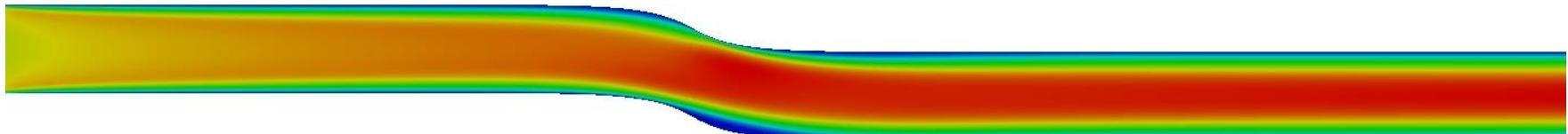
# Setting up and running an optimization case in OpenFOAM.

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Senior Researcher, NTUA

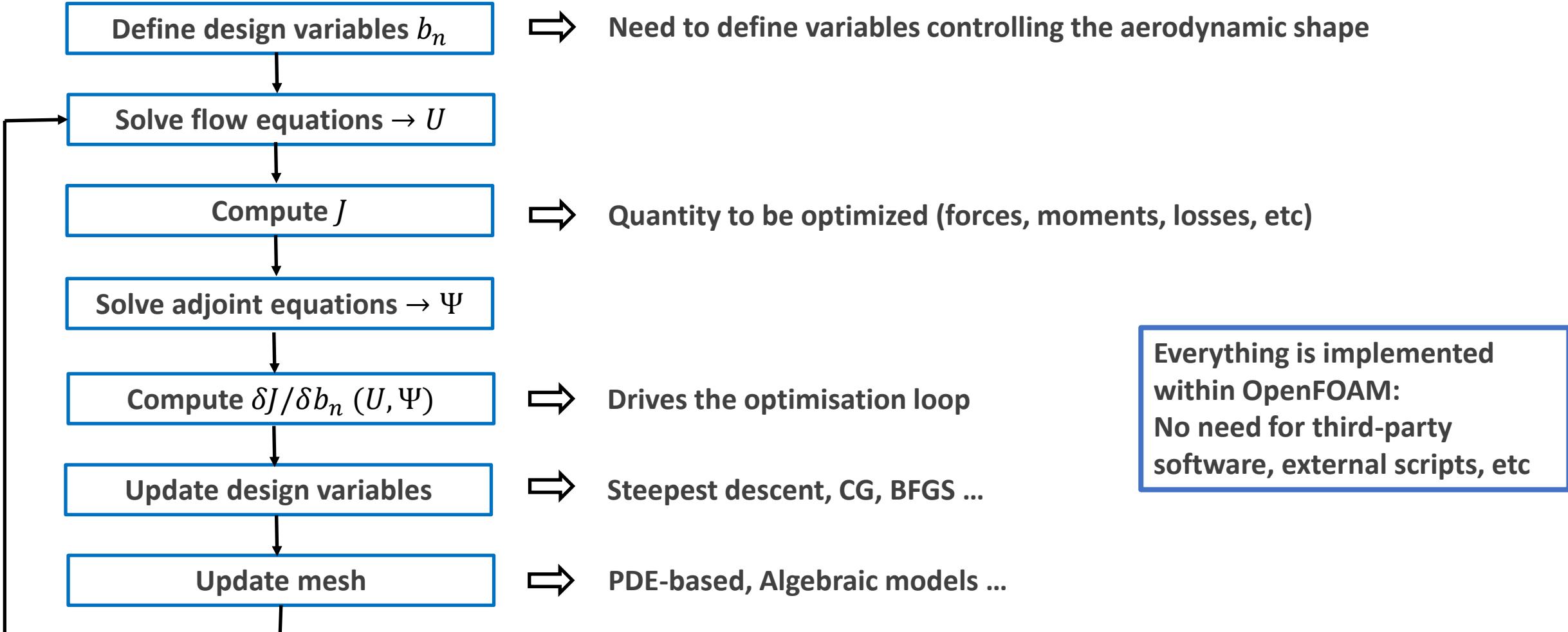
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## The tutorial case

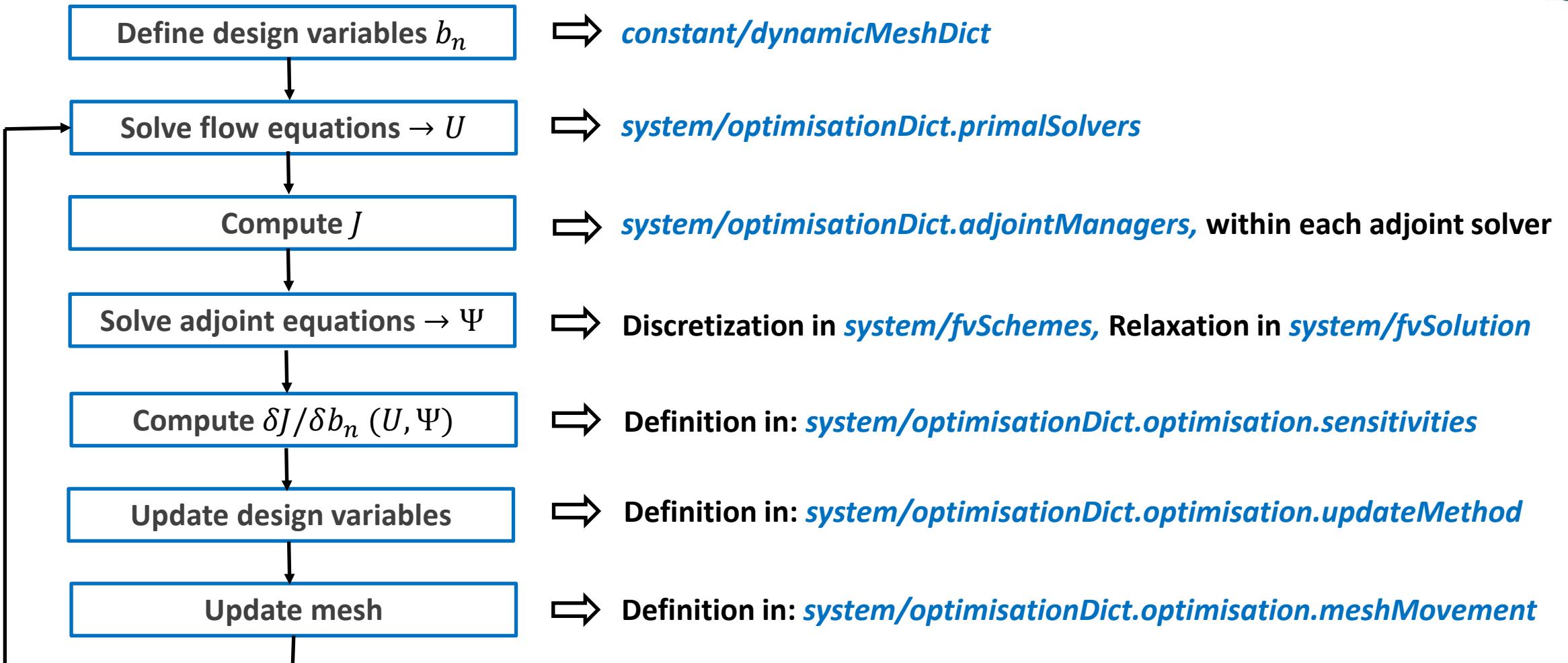
- Case is derived from  
`$FOAM_TUTORIALS/incompressible/adjointOptimisationFoam/shapeOptimisation/sbend/laminar/opt/\\unconstrained/BFGS/`  
but with a smaller mesh to get results faster
- Laminar flow within an S-bend 2D duct, mesh is provided
- $Re = 1000$
- Objective: minimize volume-weighted total pressure losses  $J = - \int_{S_{I,O}} \left( p + \frac{1}{2} v_k^2 \right) v_i n_i dS$



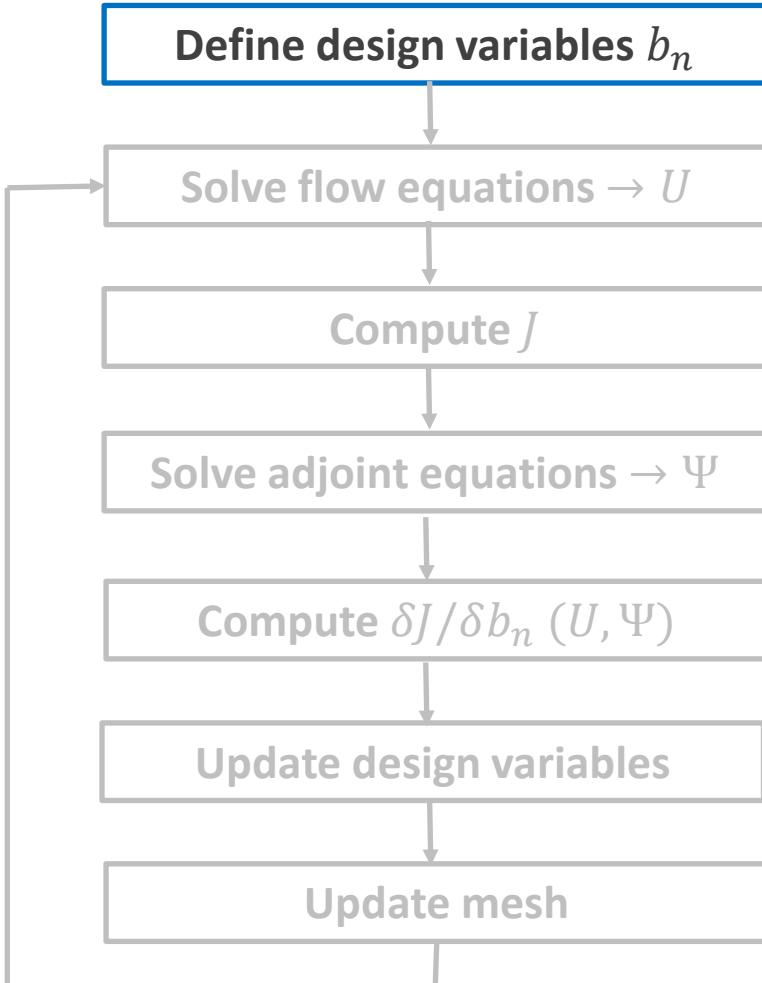
# Gradient-based Shape Optimisation Loop



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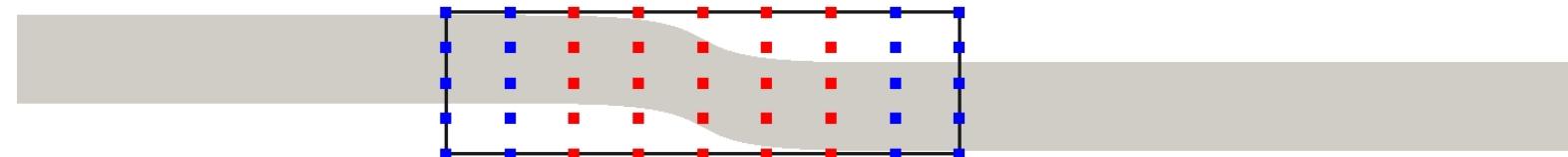


# Gradient-based Shape optimisation Loop



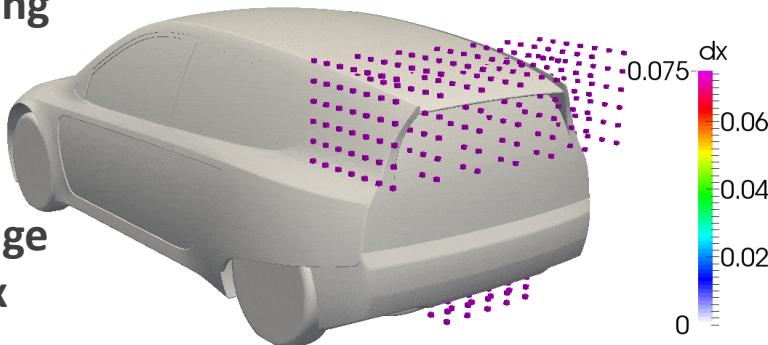
Parameterization for shape optimisation:

- NURBS Curves (2D) and Surfaces (3D)
- All of the wall nodes
- **Volumetric B-Splines (Free Form Deformation, FFD)**



Volumetric B-Splines:

- Maps all CFD grid points within the morphing boxes from the Cartesian to a parametric space  $(x, y, z) \rightarrow (u, v, w)$
- Mapping has to be done only once
- Then, changing the control points will change all CFD grid nodes within the morphing box (boundary and internal)
- Update is done through an algebraic relation: very fast!



# Gradient-based Shape optimisation Loop

## Define design variables $b_n$

Defined in: *constant/dynamicMeshDict*

```

solver volumetricBSplinesMotionSolver;
volumetricBSplinesMotionSolverCoeffs
{
    duct
    {
        type cartesian;
        nCPsU 9;
        nCPsV 5;
        nCPsW 3;
        degreeU 3; // max: nCPsU - 1
        degreeV 3; // max: nCPsV - 1
        degreeW 2; // max: nCPsW - 1
    }
    controlPointsDefinition axisAligned;
    lowerCpBounds (-1.1 -0.21 -0.05);
    upperCpBounds ( 1.1 0.39 0.15);

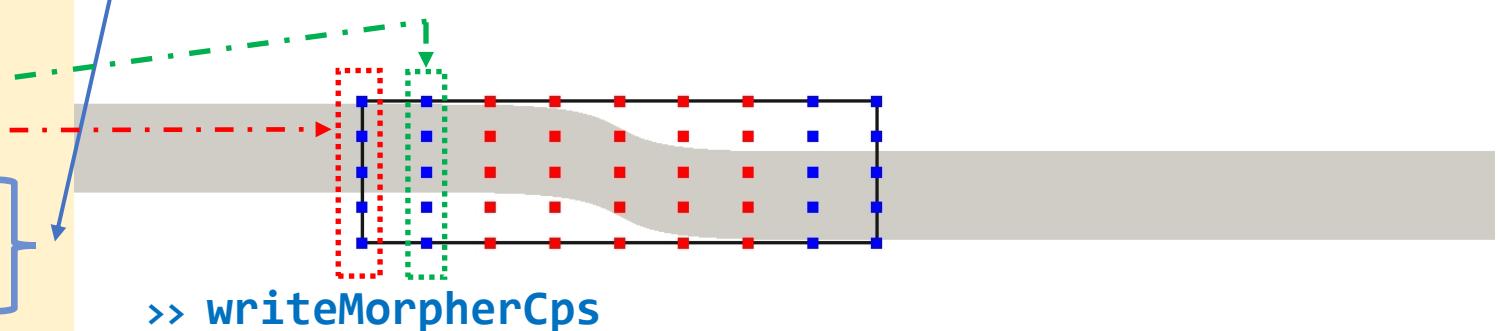
    confineUMovement false;
    confineVMovement false;
    confineWMovement true;
    confineBoundaryControlPoints false;

    confineUMinCPs ((true true true); (true true true));
    confineUMaxCPs ((true true true) (true true true));
    confineWMinCPs ((true true true));
    confineWMaxCPs ((true true true));
}

```

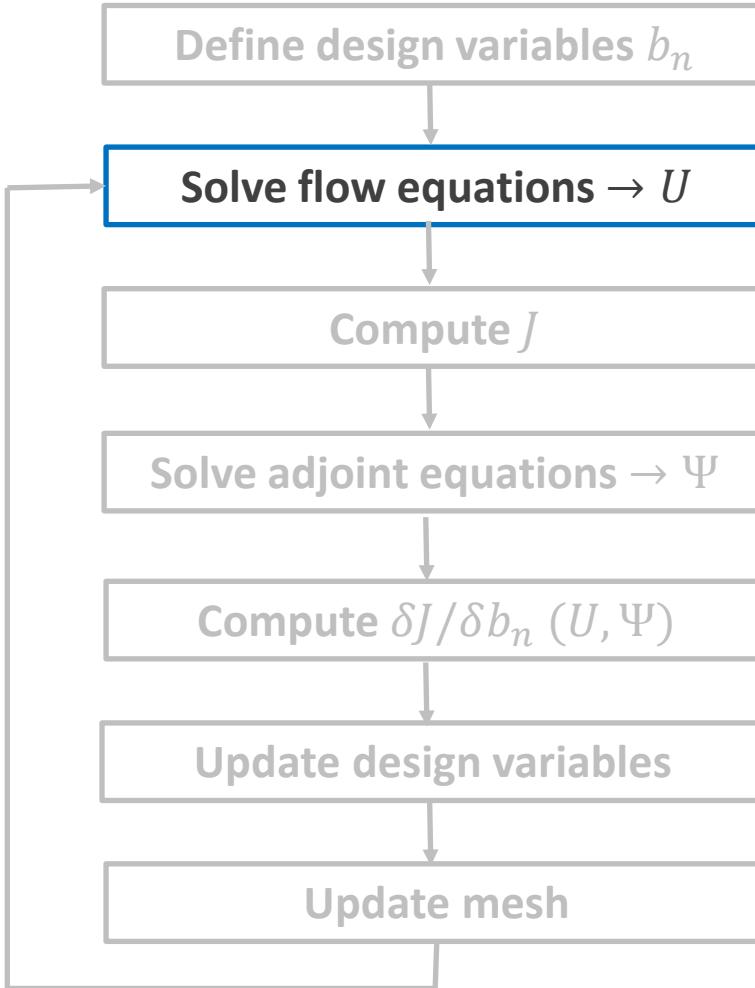
### Basic entries:

- Number of control points (CPs) per box direction
- Degree per direction (smaller degree → more local support)
- CPs defined either aligned with a coordinate system (Cartesian, cylindrical) or given manually through a dictionary
- Possible to confine the movement of (some of) the CPs in certain directions
- Continuity with the stationary part of the mesh must be preserved! Keeping the boundary CPs constant



Writes the control points in a Paraview-readable format

# Gradient-based Shape optimisation Loop



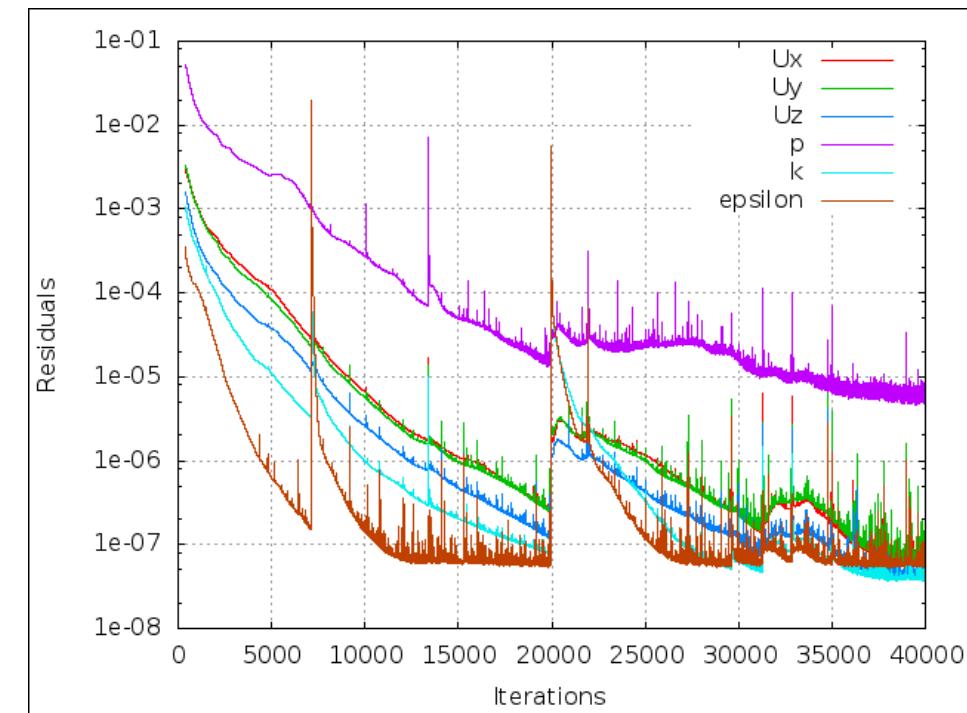
Defined in `system/optimisationDict.primalSolvers`

Incompressible, steady-state flows

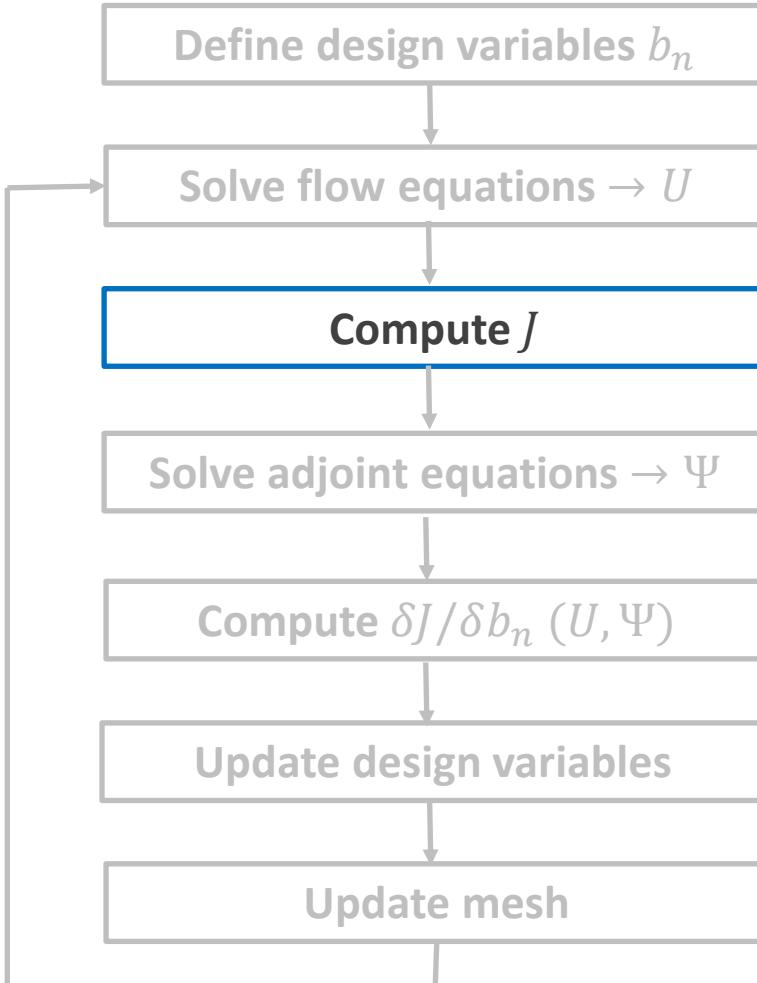
- SIMPLE is incorporated into `adjointOptimisationFoam`
- Multi-point optimisation supported; can define more than one primal solvers

Desired for optimisation, if possible

- Well converged solution (e.g. residuals of  $\sim 1.e-05$ ,  $1.e-06$ )
- Non-oscillating residuals



# Gradient-based Shape optimisation Loop



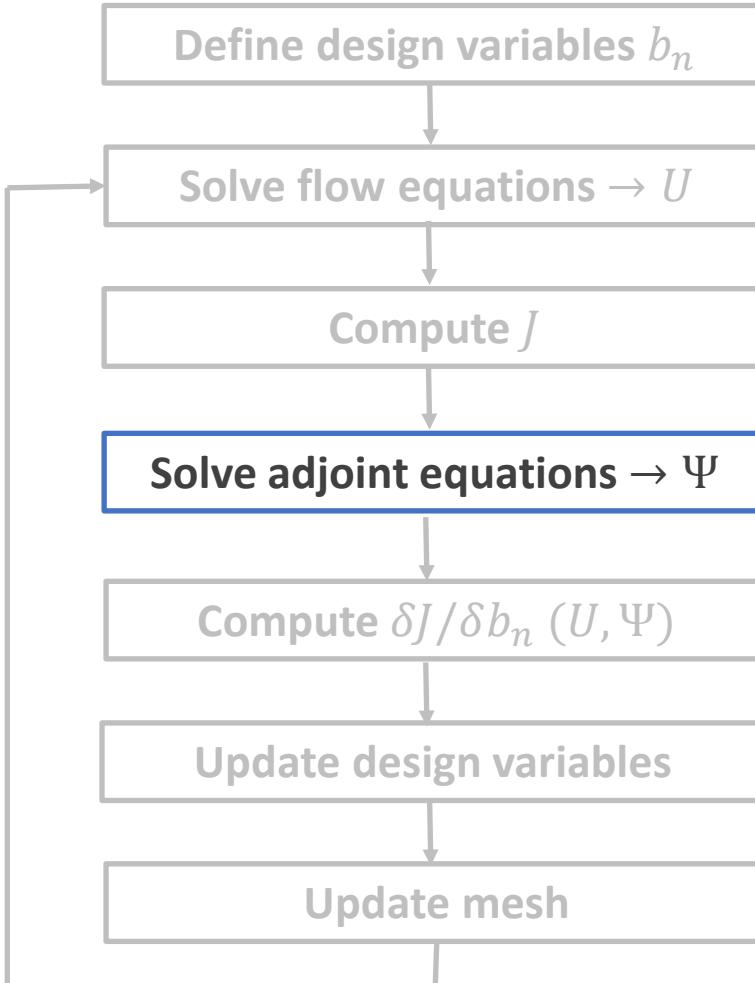
*Defined in system/optimisationDict.adjointManagers,  
within each adjoint solver*

Quantity to be optimised

- *adjointOptimisationFoam* always assumes minimization
- Objectives can be defined as (surface or volume) integral quantities
- A number of objective functions are available:  
Forces, moments, total pressure losses etc ...
- Multiple objective functions can be tackled by concatenating them into a single one using appropriate weights

$$J = w_1 J_1 + w_2 J_2$$

# Gradient-based Shape optimisation Loop



*Discretization in system/fvSchemes, Relaxation in system/fvSolution*

$$\begin{aligned}
 R^q &= -\frac{\partial u_j}{\partial x_j} + \boxed{\frac{\partial J_{\Omega'}}{\partial p}} = 0 \\
 R_i^u &= \boxed{u_j \frac{\partial v_j}{\partial x_i}} - \boxed{\frac{\partial (u_i v_j)}{\partial x_j}} - \frac{\partial \tau_{ij}^a}{\partial x_j} + \frac{\partial q}{\partial x_i} + \boxed{\frac{\partial J_{\Omega'}}{\partial v_i}} = 0, \quad i = 1, 2, 3
 \end{aligned}$$

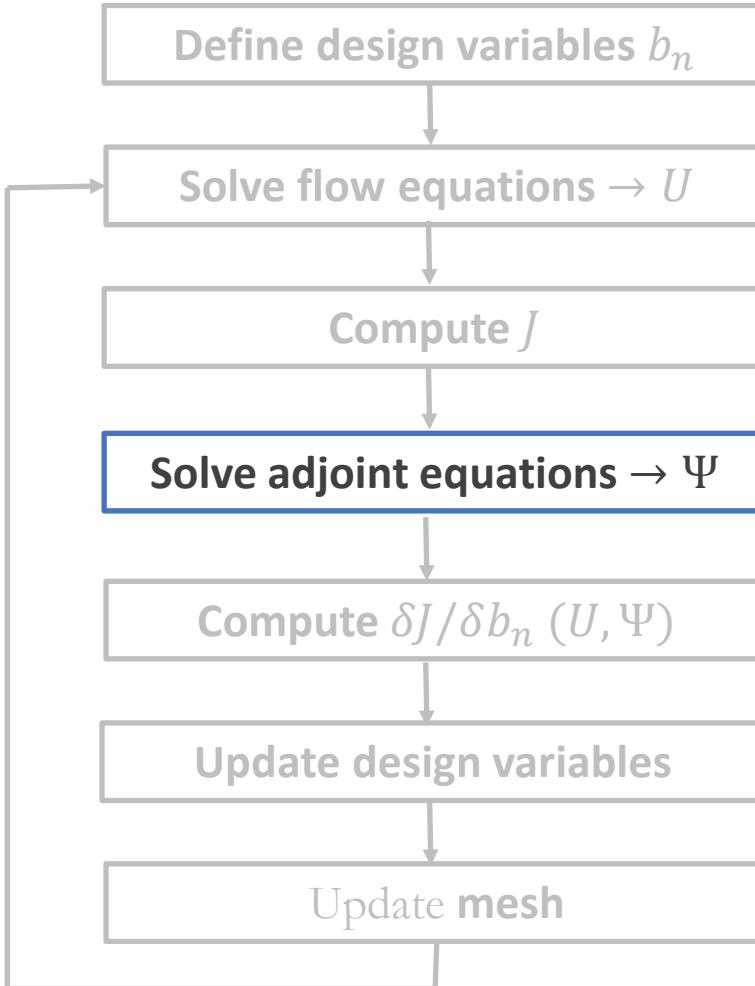
ATC                    AC

**Adjoint PDEs (laminar flows):**

- Similar form with the Navier-Stokes equations. A few noticeable differences
- Adjoint convection (AC): adjoint velocity is convected by the (minus) primal velocity. Linear equations!
- Adjoint Transpose Convection (ATC): Non-conservative term. Numerically tricky in real-word applications.
- Source terms if the objective function includes volume integrals containing  $p$  or  $v_i$

**Additional terms and equations when dealing with turbulent flows**

# Gradient-based Shape optimisation Loop



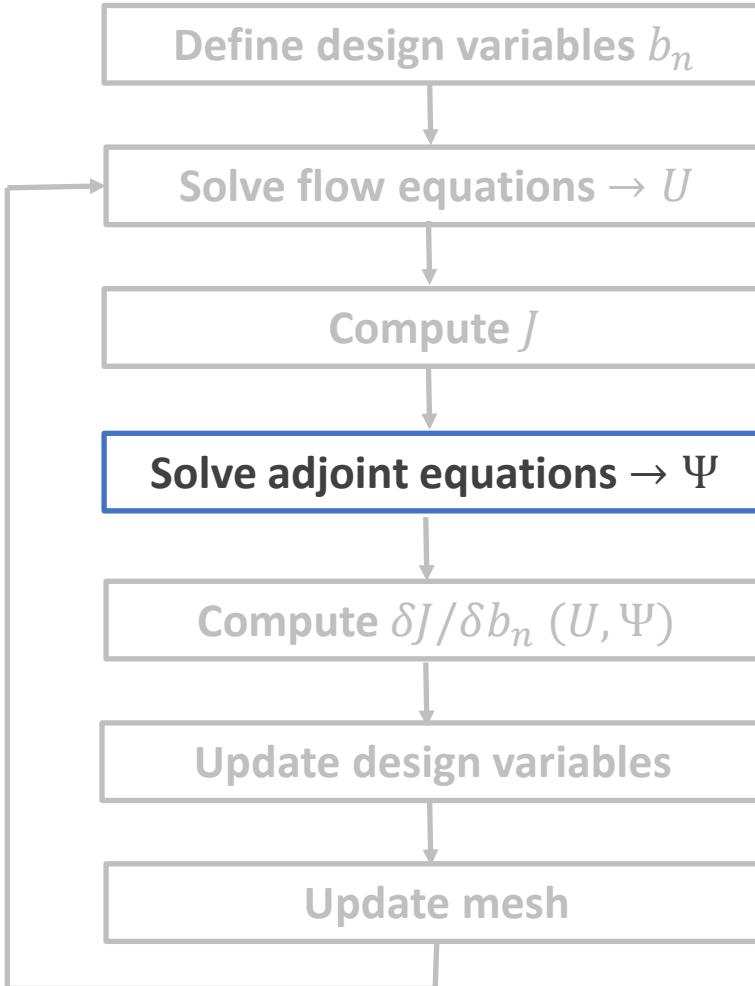
*Defined in 0/pa and 0/Ua*

$$\begin{aligned}
 u_{\langle n \rangle} &= u_j n_j = - \frac{\partial J_{S_{I-W},i}}{\partial p} n_i \\
 u_{\langle t \rangle}^I &= u_i t_i^I = \frac{\partial J_{S_{I-W},k}}{\partial \tau_{ij}} n_k t_i^I n_j + \frac{\partial J_{S_{I-W},k}}{\partial \tau_{ij}} n_k t_j^I n_i \\
 u_{\langle t \rangle}^{II} &= u_i t_i^{II} = \frac{\partial J_{S_{I-W},k}}{\partial \tau_{ij}} n_k t_i^{II} n_j + \frac{\partial J_{S_{I-W},k}}{\partial \tau_{ij}} n_k t_j^{II} n_i
 \end{aligned}$$

**Adjoint Boundary conditions:**

- Depend on the type (**not value!**) of primal boundary conditions!
- Most common for incompressible flows: Dirichlet Inlet  $\vec{v}$ , Dirichlet Outlet  $p$
- Depend on the derivatives of  $J$  w.r.t. the pressure, velocity and stress tensor

# Gradient-based Shape optimisation Loop

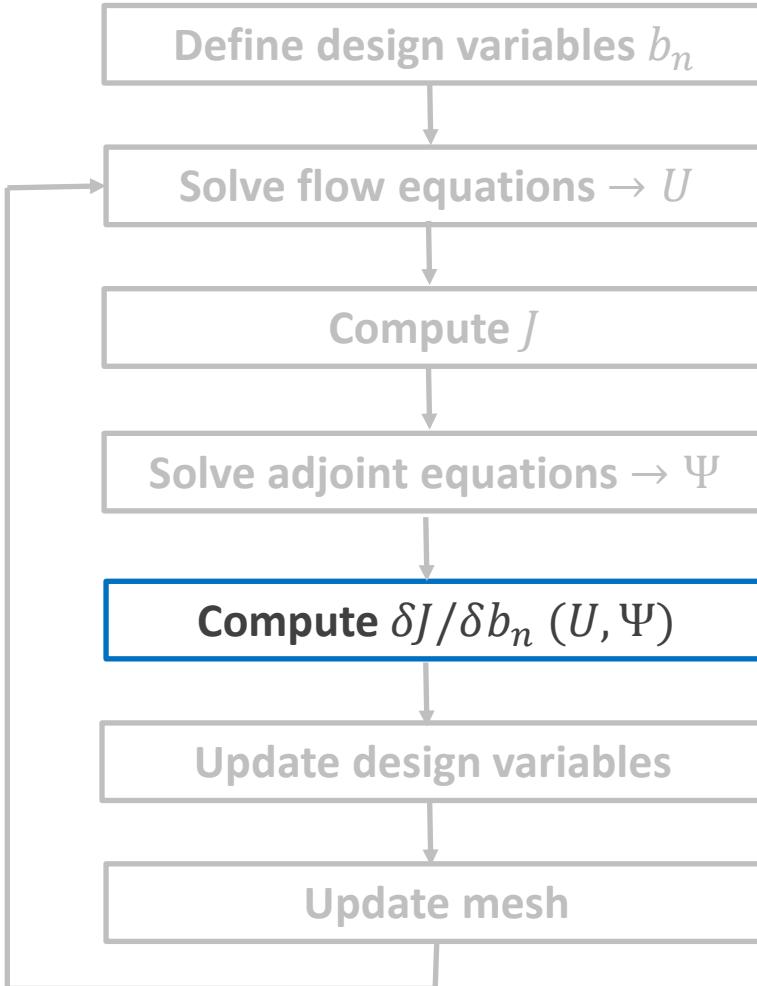


Defined in *system/optimisationDict.adjointManagers*

How many adjoint equations do we have to solve?

- One for each objective for which we need the gradient
  - Gradients of linear combinations of functions defined at a single operating point can be computed with one adjoint solution!
  - Advanced methods dealing with constraints (e.g. SQP, constraint projection) need the gradient of the constraint function separately
- (At least) One for each operating point solved

# Gradient-based Shape optimisation Loop



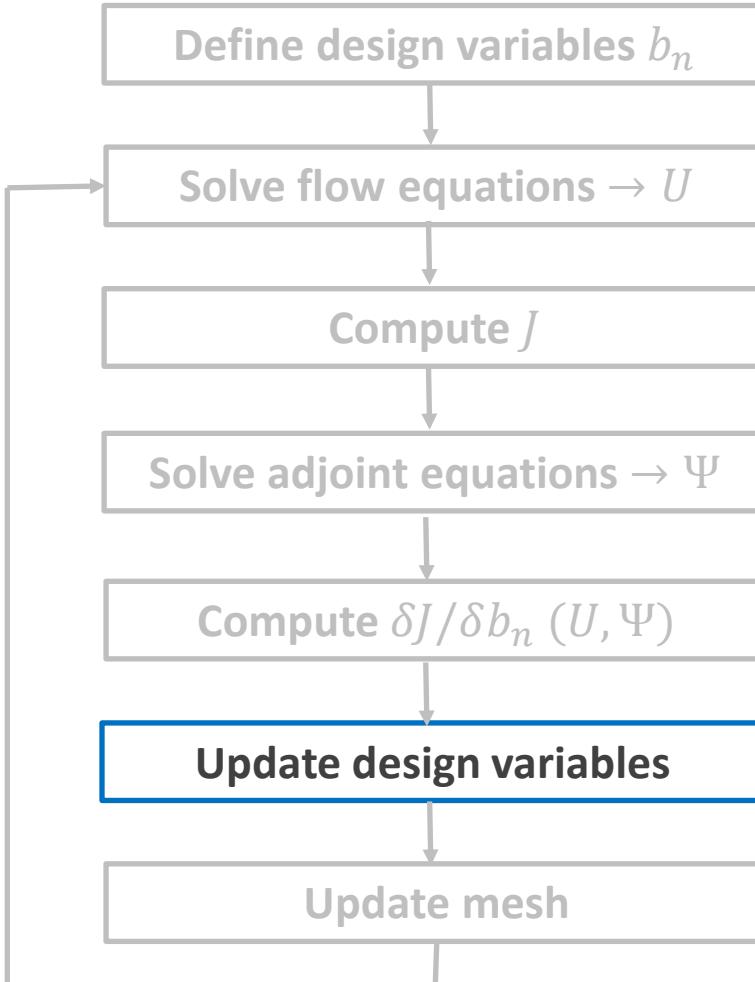
Defined in

*system/optimisationDict.optimisation.sensitivities*

Two mathematical formulations for shape optimisation

- Based on Surface Integrals, (E)-SI
  - Need to solve an additional adjoint grid displacement PDE for  $m_i^a$ 
    - Boundary conditions are created automatically
    - Need to define a linear solver in *fvSolution*
    - No relaxation is required
    - Solved at a post-processing level, i.e. after the solution of the adjoint mean flow equations
- Based on Field Integrals, FI
  - Need to compute the grid sensitivities fields, i.e.  $\frac{\delta x_k}{\delta b_n}$
  - Depending on the grid displacement model this might be computed by
    - solving additional PDEs (e.g. PDE-based grid displacement)
    - Analytically (e.g. Volumetric B-Splines)

# Gradient-based Shape optimisation Loop



Defined in

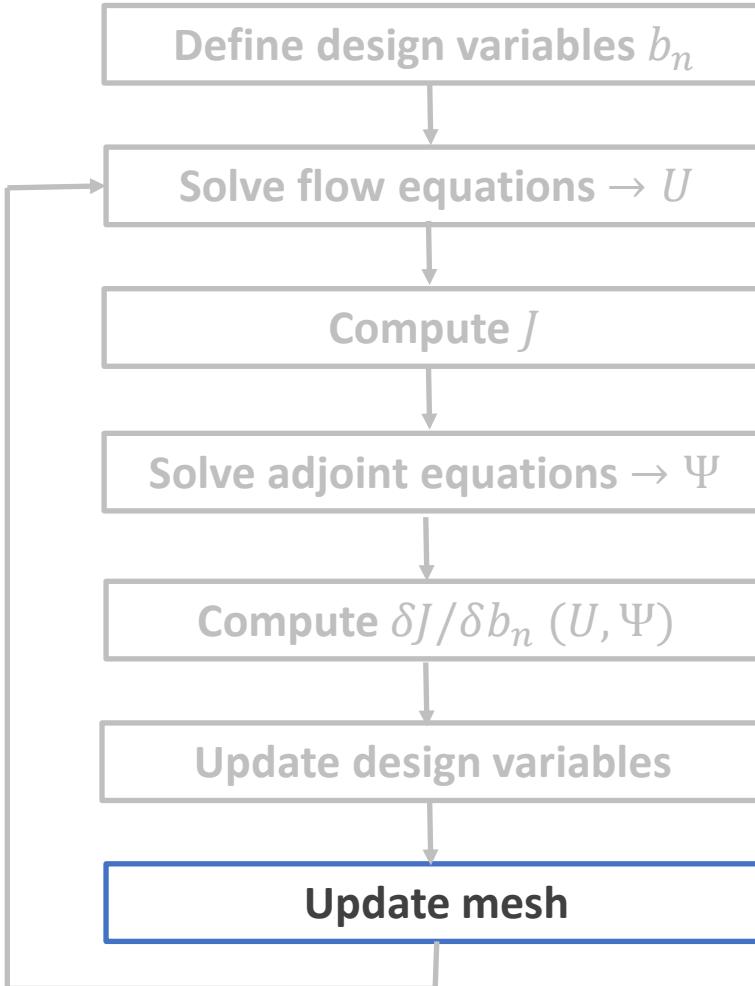
*system/optimisationDict.optimisation.updateMethod*

Compute the update of the design variables based on  $\frac{\delta J}{\delta b_n}$  through

$$b_n^{new} = b_n^{old} + \eta s_n$$

- Unconstrained optimisation
  - Steepest descent
  - Conjugate Gradient
  - Quasi-Newton methods: BFGS, SR1
- Constrained optimisation
  - Constraint projection (exceptional for linear constraints)
  - SQP
- Step ( $\eta$ ) definition
  - Direct (usually not practical)
  - Through a max. desired deformation in the initial opt. cycle

# Gradient-based Shape optimisation Loop



**Defined in**  
*constant/dynamicMeshDict*

- Need to translate  $\Delta b_n$  into a new geometry and computational mesh
- Remeshing can be costly and possibly result to inconsistent sensitivity derivatives. Grid displacement is preferable
- Depends on the parameterization and chosen grid displacement method
  - Usually, one tool for parameterization (e.g. NURBS), a different one for grid displacement (e.g. Laplace PDEs)
  - Volumetric B-Splines handles both simultaneously
- **checkMesh** ran after each update to check mesh quality

## S-bend: optimisation results

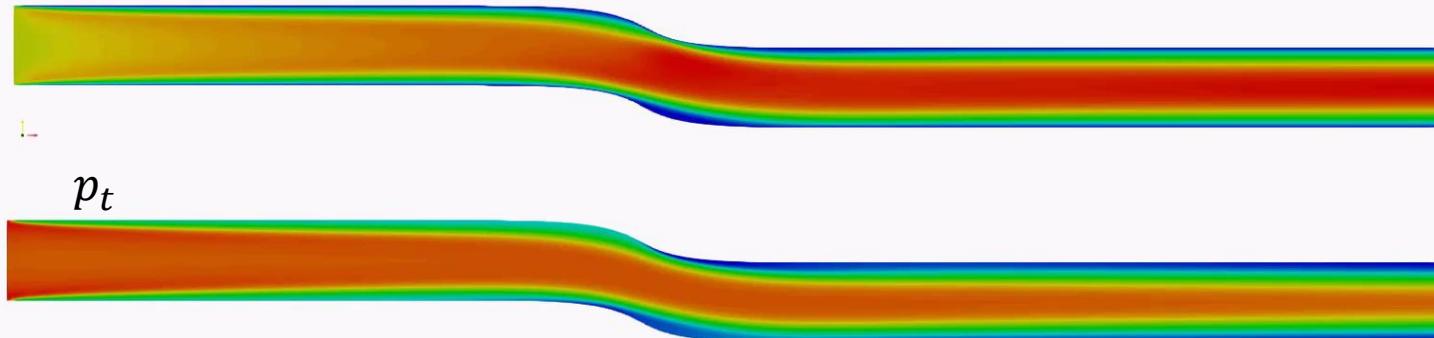
Run the optimization loop

```
>> ./Allrun.parallel > log 2> err & (~2.5  
min/4 procs)
```

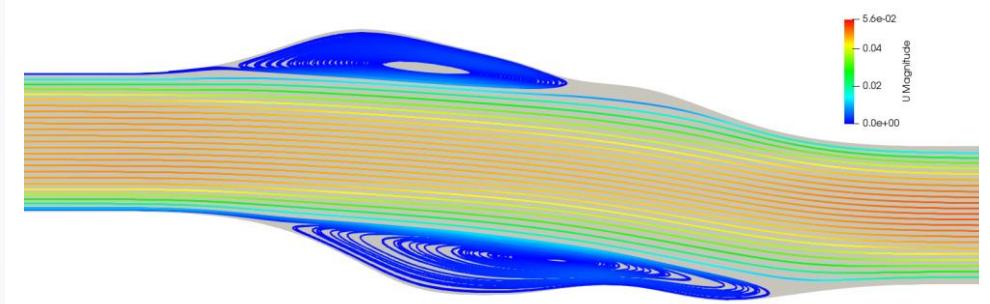
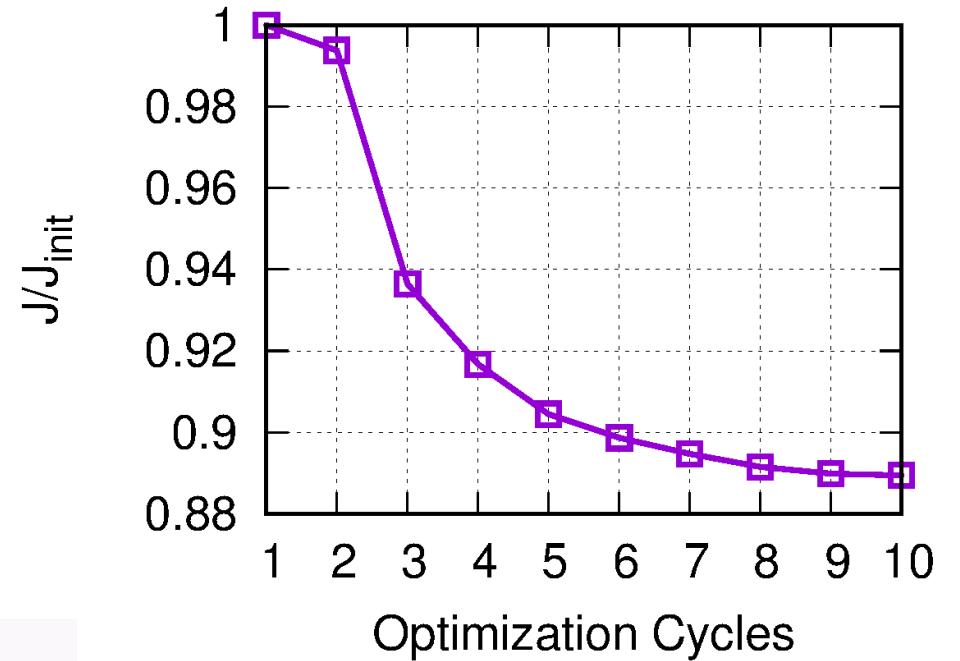
What to examine:

- Is  $J$  reduced?
- Is  $J$  converged? (history in *optimisation/objective* folder)
- Have the flow equations converged? (check log file)
- Is the mesh valid at the optimised solutions? (check log file or checkMesh)
- What is the mechanism behind the reduction in  $J$ ?
- **Don't be afraid of exotic solutions!**

$|\vec{v}|$

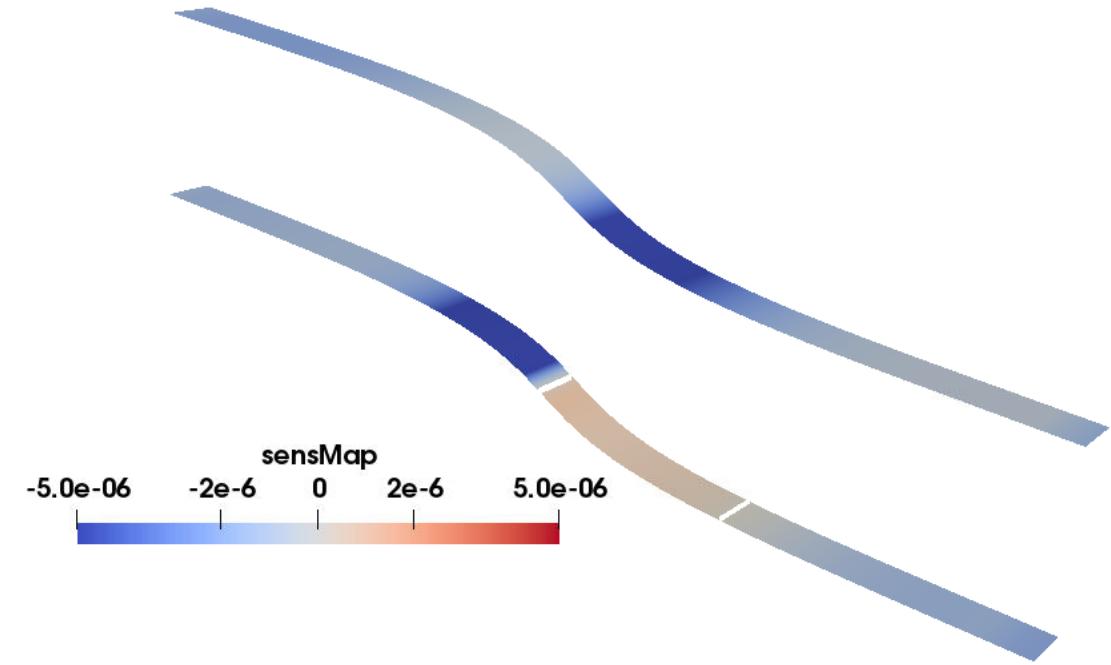


$p_t$



## S-bend: Computing sensitivity maps

- Compute  $\frac{\delta J}{\delta x_i} n_i$
- A few changes in *optimisationDict* and *controlDict*
- Tells us how each boundary node has to move to reduce  $J$ 
  - Red: move against the surface normal (inwards)
  - Blue: move towards the surface normal (outwards)
  - White-ish: insignificant
- Computed on the initial geometry: does not mean that the optimised geometry will follow this ! ...
- Good feedback towards the designer
- Useful in placing morhing boxes

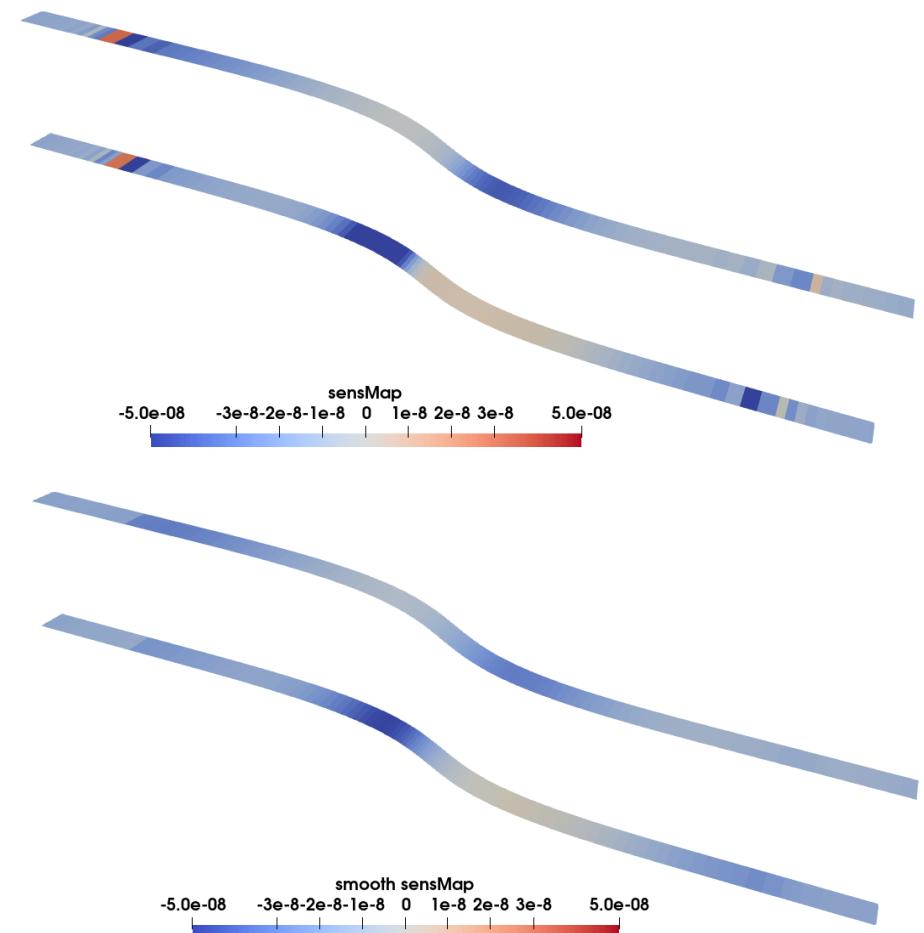


## S-bend: Smoothing the sensitivity map

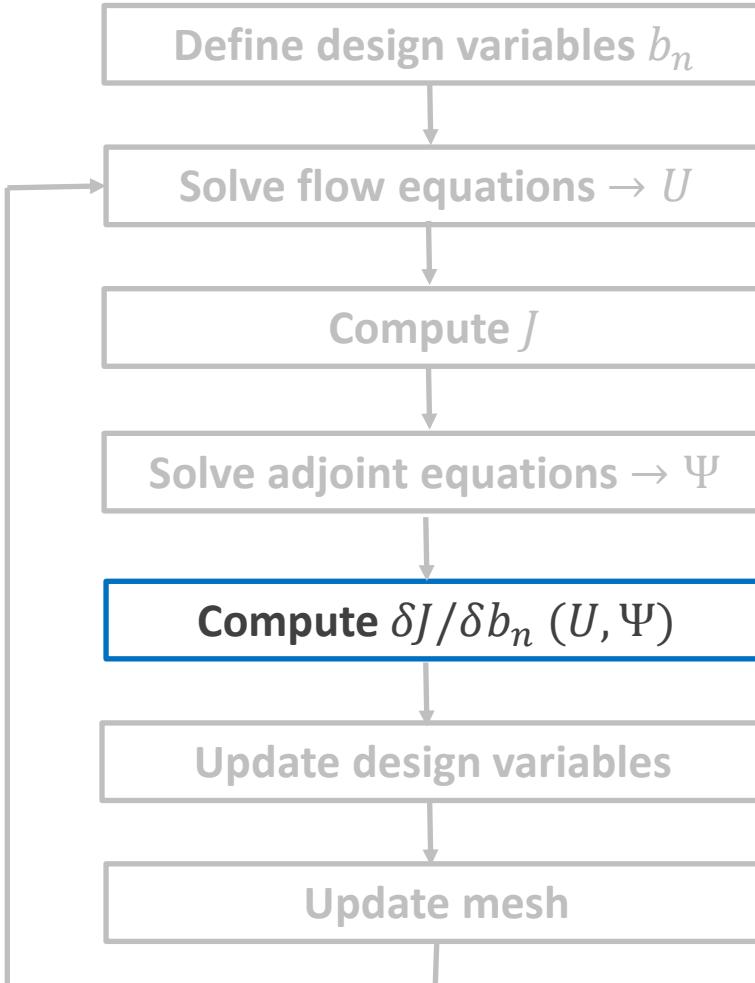
- In more complex/industrial cases, checkerboards occur in the computed sensitivity maps.
- This problem becomes pronounced in meshes built with `snappyHexMesh`!
- The direction of favorable surface displacement becomes ambiguous...
- Smooth the sensitivity-map,  $G$ , by solving

$$-R^2 \frac{\partial^2 \hat{G}}{\partial x_j^2} + \hat{G} = G$$

on a `finiteArea` mesh.



# S-bend: Smoothing the sensitivity map – Additional Entries



- Additional entries in ***system/optimisationDict.optimisation.sensitivities*** related to the Laplace-Beltrami equation
 
$$-R^2 \frac{\partial^2 \hat{G}}{\partial x_j^2} + \hat{G} = G$$
- The smoothing radius is either specified explicitly, or computed as a multiple of the average surface edges' length.
- Boundary conditions for the smooth sensitivity field are created automatically.
- For the creation of the ***faMesh***, an ***faMeshDefinition*** dictionary can be optionally provided in the ***system*** folder.
- faSchemes*** & ***faSolution*** should be present in the ***system*** directory.

## Takeaway messages:

- Adjoint supports optimisation loops at a small CPU cost ( $\sim 20$  cycles  $\rightarrow \sim 40$  flow solutions)
- Ideal for both early-stage development and refinement
- More optimisation types available
  - Active flow control (jet-based optimisation)
  - A Posteriori Error Analysis (optimally refine your mesh to compute an accurate objective)
  - Design under uncertainties
- Optimisation (like CFD) is not magic. Take care when defining your problem
- Before accepting (or discarding) an optimised geometry
  - Check the convergence of the flow equations
  - Check the mesh quality
- Try to understand the mechanisms behind the objective reduction
  - Often leads to better designs and/or better-defined optimisation problems!

Additional topics covered through the tutorials under  
**\$FOAM\_TUTORIALS/incompressible/adjointOptimisationFoam**

- Effect of the update method  
**shapeOptimisation/sbend/laminar/opt/unconstrained**
- Constrained optimisation  
**shapeOptimisation/naca0012/lift/opt/constraintProjection**
- 3D, industrial-like cases  
**shapeOptimisation/motorbike**



When in doubt about the case settings, you can consult the manual